

Long Glass Fiber Orientation in Thermoplastic Composites Using a Model that Accounts for the Flexibility of the Fibers

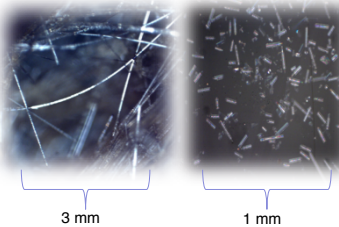
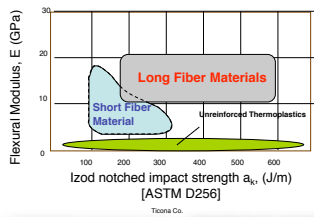
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Motivation for Research

Create fiber reinforced materials as a function of injection-molding design for:

- Increased strength properties
- Production of relatively light weight materials
- More energy efficient transportation

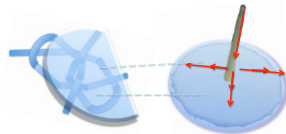
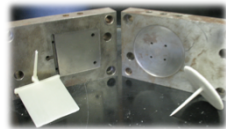


Scope of Research

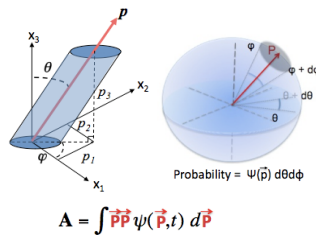
- Implement and evaluate current/new theories to model fiber orientation in complex flow
- Evaluate model parameters from rheological experiments
- Implement the use of stable numerical methods based on the discontinuous Galerkin Finite element method

$$v_r(r,z) = \frac{3\dot{Q}}{8\pi h r} \left[1 - \left(\frac{z}{h}\right)^2 \right]$$

$$v_z(r,z) = 0$$



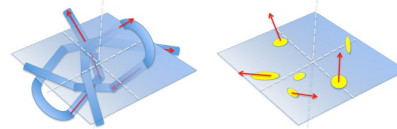
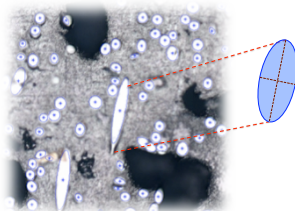
Obtain velocity field and solve fiber orientation in an uncoupled manner. How do we model fiber orientation?



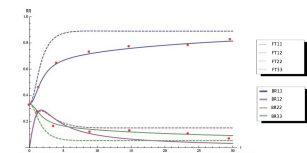
$$A = \begin{bmatrix} 1/3 & 0 & 0 \\ 0 & 1/3 & 0 \\ 0 & 0 & 1/3 \end{bmatrix} \quad A = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Random Fully ordered in x_1 -direction

Obtain fiber orientation from polished micrographs using a digital imaging technique



A single flexible (long) fiber possibly exhibits many orientations in different planes. Rigid (short) fibers exhibit only one set of orientation data along its length.



Long transient behavior, consistent with experiment, can be explained via the Bead-Rod model by attributing this behavior to fiber flexibility.

Folgar Tucker Model

$$\frac{DA}{Dt} = \left[\underline{A} \cdot \underline{\kappa}^T + \underline{\kappa} \cdot \underline{A} - 2 \underline{D} : \underline{A} + 2C_1 U_D (\delta - 3\underline{A}) \right]$$

Generalized Jeffery for Fibers Folgar-Tucker Term

Though popularly used for short fiber simulations, we want to know how this model performs when being used to predict long fiber orientation.

What about a model that accounts for fiber flexibility?

Bead-Rod Model

$$\underline{A} = \int \hat{p} \hat{p} \psi(\hat{p}, \theta, t) d \hat{p} d \theta$$

$$\underline{B} = \int \hat{p} \hat{p} \psi(\hat{p}, \theta, t) d \hat{p} d \theta$$

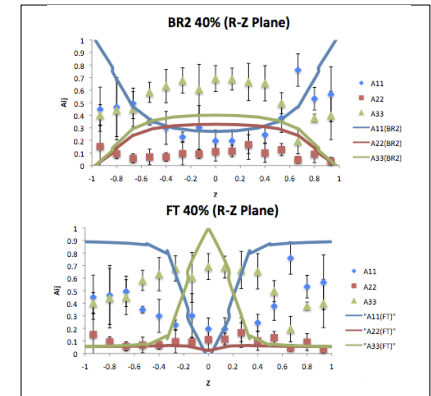
$$\underline{C} = \int \hat{p} \psi(\hat{p}, \theta, t) d \hat{p} d \theta$$

$$\frac{DA}{Dt} = \underline{A} \cdot \underline{\kappa}^T + \underline{\kappa} \cdot \underline{A} - [(\underline{\kappa} + \underline{\kappa}^T) : \underline{A}] \underline{A} + \frac{l_B}{2} [\underline{C} \underline{\mu} + \underline{\mu} \underline{C} - 2(\underline{\mu} \cdot \underline{C}) \underline{A}] - 2k[\underline{B} - \underline{A} \text{tr}(\underline{B})]$$

$$\frac{DB}{Dt} = \underline{B} \cdot \underline{\kappa}^T + \underline{\kappa} \cdot \underline{B} - [(\underline{\kappa} + \underline{\kappa}^T) : \underline{A}] \underline{B} + \frac{l_B}{2} [\underline{C} \underline{\mu} + \underline{\mu} \underline{C} - 2(\underline{\mu} \cdot \underline{C}) \underline{B}] - 2k[\underline{A} - \underline{B} \text{tr}(\underline{B})]$$

$$\frac{DC}{Dt} = \underline{\kappa} \cdot \underline{C} - (\underline{A} : \underline{\kappa}) \underline{C} + \frac{l_B}{2} [\underline{\mu} \cdot \underline{C} - (\underline{\mu} \cdot \underline{C}) \underline{C}] - k \underline{C} [1 - \text{tr}(\underline{B})]$$

$$\underline{\mu} = \sum_{i=1}^3 \left(\sum_{j=1}^3 \sum_{k=1}^3 \frac{\partial^2 v_j}{\partial x_i \partial x_k} A_{jk} \right) \underline{e}_i$$



Conclusions and Future Work

- Long fiber composites exhibit flexibility
- Transient behavior can be explained by the Bead-Rod model via flexibility within the model
- Long fiber orientation in complex flow is broader than predicted by Folgar Tucker
- Bead-Rod model parameters must be fit from rheology in the near future
- More complex flow data is needed for long fibers to affirm the Bead-Rod model's validity

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